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DEPARTMENT OF DEFENSE LAND FALLOUT  
PREDICTION SYSTEM. VOLUME II: INITIAL  
CONDITIONS, SUPPLEMENT

Hillyer G. Norment

Mount Auburn Research Associates, Incorporated

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VOLUME II  
INITIAL CONDITIONS  
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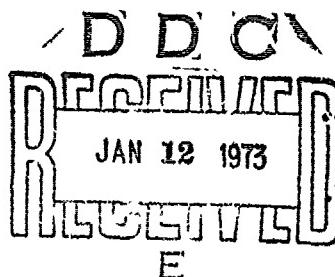
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13. ABSTRACT <p>The DELFIC Initial Conditions Module code has been revised to meet the requirements of the new DELFIC fallout prediction system. This documentation supplement describes the revised code. Discussion of the revised code emphasizes particle size distributions. The code can accept parameters that define lognormal or power-law distributions, or it can accept a distribution in tabular form. Details necessary for use of the code are presented. FORTRAN statement listings of revised subroutines are included.</p> <p style="text-align: center;">Ia</p>		

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II

TABLE OF CONTENTS

	<u>Page</u>
1. INTRODUCTION	1
2. THE LOGNORMAL DISTRIBUTION	3
3. THE POWER-LAW DISTRIBUTION	11
4. TABULAR DISTRIBUTIONS	15
5. USER INFORMATION	17
6. FORTRAN STATEMENT LISTINGS	21
REFERENCES	30

III

## 1. INTRODUCTION

Since publication of DASA-1800-II<sup>(1)</sup> in 1966, the Defense Land Fallout Interpretative Code (DELFIC) has undergone substantial revision in all of its modules. These revisions have created some new demands on the Initial Conditions Module (ICM) and removed some old restrictions. Of most direct consequence to the ICM are changes in the Cloud Rise Module (CRM)<sup>(2)</sup>.

The new CRM accounts for wind shear effects on the cloud rise dynamics. Therefore, shot-time winds above ground zero are input via the ICM rather than via the Cloud Rise-Transport Interface Module (CRTIM) as was done originally. The old CRM could accept no more than forty particle size classes, and the size class structure was rigidly prescribed. These restrictions have been relaxed in the new CRM, and the ICM has been revised accordingly. In addition, the ICM has been given a capability to accept parameters that define a power-law particle size distribution function. From these parameters, it constructs a particle size class table with a user-specified number of entries.

Subroutines LINK1 and DSTBN have been revised, and a new subroutine, SHWIND, which is called by LINK1, has been created. Subroutines MASS, TEMP, TIME, and VAPOR remain unchanged.

Subroutine LINK1 is the ICM executive program. Subroutine DSTBN constructs particle size class tables for lognormal and power-law particle distributions. Subroutine SHWIND reads in the shot-time winds above ground zero.

The logic of the ICM consists of a card input, which is described in Table 1, followed by serial exercise of the subordinate subroutines. Adequate detailed documentation is provided by the FORTRAN statement listings.

Use of the ICM is quite simple with one exception: definition of particle size distributions. Therefore, the bulk of this supplement is devoted to discussions of particle size distributions.

## 2. THE LOGNORMAL DISTRIBUTION

### 2.1 Fundamentals

A variable  $x$  is said to be normally distributed if the probability of its occurrence in the range  $x$  to  $x + dx$  is given by

$$dN(x|\mu, \sigma^2) = \frac{1}{\sigma\sqrt{2\pi}} \exp\left[-\frac{1}{2}\left(\frac{x-\mu}{\sigma}\right)^2\right] dx, \quad (1)$$

where  $\mu$  is the mean value of  $x$  and  $\sigma^2$  is the variance of  $x$ . The square root of the variance,  $\sigma$ , is called the standard deviation.

To define a lognormal distribution, we make the transformation

$$x = \ln(y) . \quad (2)$$

In terms of the variable  $y$  Eq. (1) becomes

$$dN(y|\mu, \sigma^2) = \frac{1}{\sigma\sqrt{2\pi}} \exp\left[-\frac{1}{2}\left(\frac{\ln y - \mu}{\sigma}\right)^2\right] d(\ln y), \quad (3)$$

and  $y$  is said to be lognormally distributed. <sup>(3)</sup>

Some statistical properties of  $y$  are as follows:

$$\text{mean}(y) = \exp(\mu + \frac{1}{2} \sigma^2) \quad (4)$$

$$\text{median}(y) = \exp(\mu) \quad (5)$$

$$\text{mode}(y) = \exp(\mu - \sigma^2) \quad (6)$$

$$\text{variance}(y) = [\exp(\sigma^2) - 1] \exp(2\mu + \sigma^2). \quad (7)$$

Let  $\bar{y}$  and  $s$  be the geometric mean and geometric standard deviation of  $y$ . Then

$$\bar{y} = \text{median}(y) = \exp(\mu) \quad (8)$$

and

$$s = \exp(\sigma) . \quad (9)$$

Let  $\lambda'_j$  be the  $j$ -th moment of  $\Lambda(y|\mu, \sigma^2)$  about the origin. Then by definition

$$\lambda'_j = \int_0^\infty y^j d\Lambda(y|\mu, \sigma^2) , \quad (10)$$

and from the properties of the normal distribution it follows that

$$\lambda'_j = \exp(j\mu + \frac{1}{2} j^2 \sigma^2) . \quad (11)$$

A feature that distinguishes the lognormal distribution from the normal distribution is the existence of moment distributions. The  $j$ -th moment distribution is defined as

$$\Lambda(y|\mu, \sigma^2)_j = \frac{1}{\lambda'_j} \int_0^y t^j d\Lambda(t|\mu, \sigma^2) , \quad (12)$$

which can be shown to be<sup>(3)</sup>

$$\Lambda(y|\mu, \sigma^2)_j = \Lambda(y|\mu + j\sigma^2, \sigma^2) . \quad (13)$$

The moment distributions provide simple relationships between log-normal distributions of number, surface area, and volume of particles with respect to their diameters.

## 2.2 Application to Particle Distributions

In discussions of lognormal particle distributions, confusion frequently arises because distinction is not clearly made between  $\mu$  and  $y$  and between  $\sigma$  and  $s$ . Since particular values of  $\mu$  and  $\sigma$  depend on the base of the logarithms used, we have chosen to confine our discussions in the DELFIC documentation to parameters in the form of  $y$  and  $s$ .

Suppose that we have plotted cumulative numbers of particles versus diameter on log-probability graph paper and have obtained the curve shown in Figure 1. This straight-line curve indicates that the distribution of particle number with respect to diameter,  $D$ , is lognormal. Thus,  $D$  is equivalent to  $y$  in Eq. (3), and from Eqs. (8) and (9) we have

$$y = D_{50}$$

and

$$s = D_{84.13}/D_{50}$$

These are the quantities DMEAN and SD, respectively, that are required as input to subroutine LINK1, and that are printed by LINK1. DMEAN is expressed in units of micrometers. (In words, DMEAN is the median particle diameter in the distribution of numbers of particles with respect to their diameters.) If the user specifies a lognormal distribution but does not input values for DMEAN and SD, the program supplies the values<sup>(1)</sup>:

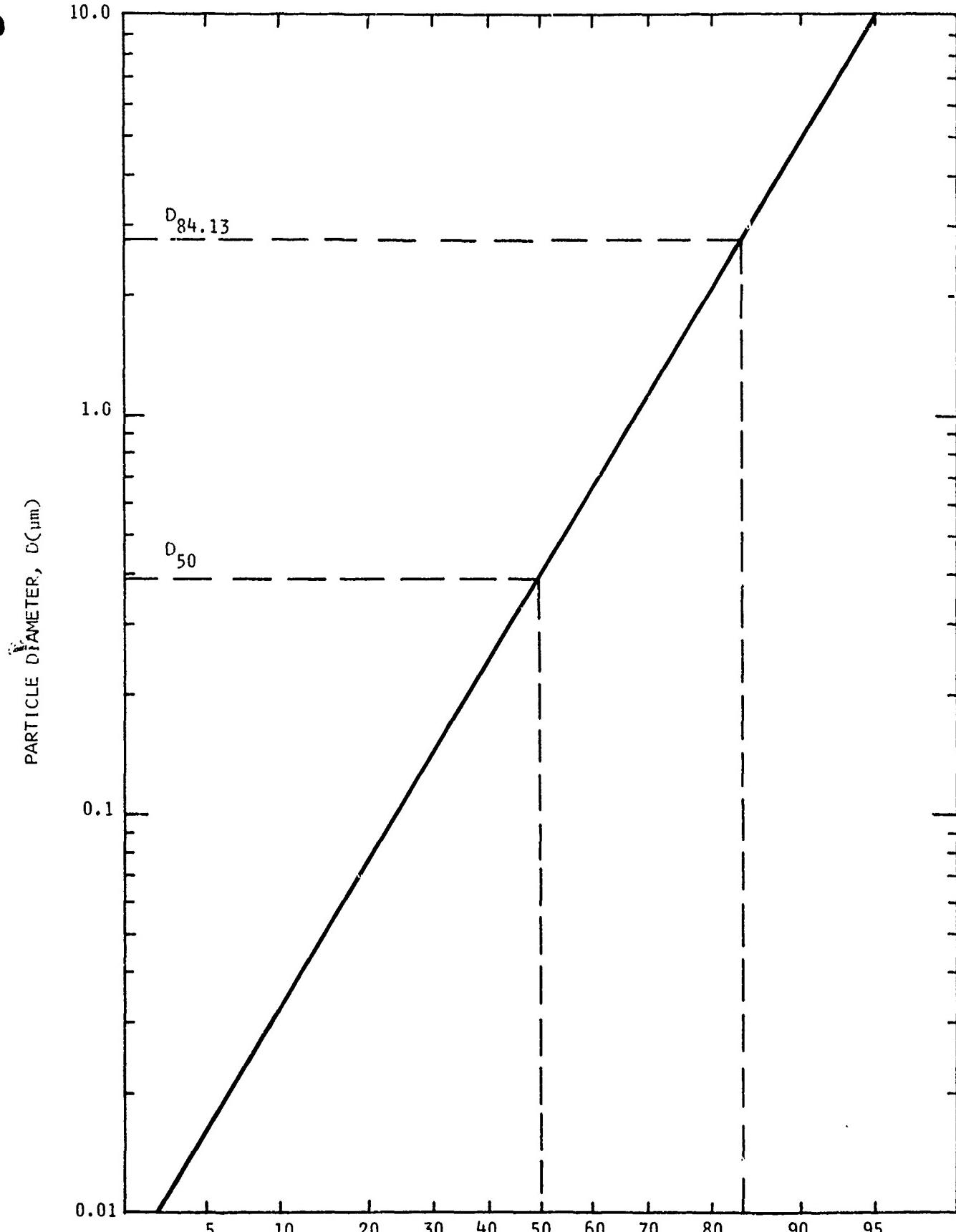


FIGURE 1. CUMULATIVE FREQUENCY GRAPH OF LOGNORMALLY DISTRIBUTED PARTICLES

DMEAN =  $\underline{y} = 0.407 \mu\text{m}$

SD =  $s = 4.0$

As noted above, the properties of the moment distributions are useful in interrelating distributions of particle number, surface area, and volume with respect to particle diameter. This is because the number distribution is the zeroth moment distribution with respect to diameter, surface area is distributed via the second moment distribution, and volume is distributed via the third moment distribution. Thus, if we assume spherical particles and if the parameters  $\mu$  and  $\sigma$  are known for either the particle number, or particle area, or particle volume distribution with diameter, then the other distributions can be determined from the equations below. The parameter  $\sigma$  is the same for all three distributions. If we use N, S, and V as subscripts to denote number, surface area, and volume, respectively, we have from Eq. (13)

$$\mu_S = \mu_N + 2\sigma^2$$

$$\mu_V = \mu_N + 3\sigma^2$$

where  $\mu$  and  $\sigma$  are related to  $\underline{y}$  and  $s$  by Eqs. (8) and (9).

If base 10 logarithms are used instead of natural logarithms, we distinguish the distribution parameters by use of primes,  $\mu'_N$  and  $\sigma'$ , and the relations become

$$\mu'_S = \mu'_N + 2\ln(10)(\sigma')^2$$

$$\mu'_V = \mu'_N + 3\ln(10)(\sigma')^2$$

where  $\ln(10) = 2.3026$ .

The distribution of particle mass with respect to diameter is taken to be equivalent to the volume distribution with respect to diameter. This implies that all particles have the same density.

### 2.3 Particle Size Class Tables

For computation purposes, the continuous lognormal distribution is replaced by a histogram. The computer program, via subroutine DSTBN, does this automatically by use of the distribution parameters and the number of size classes, NDSTR, which is input by the user.

The user specifies parameters DMEAN, SD, and NDSTR. From these, the parameters  $\mu_N$ ,  $\sigma$ , and  $\mu_V$  are determined via

$$\mu_N = \ln(DMEAN)$$

$$\sigma = \ln(SD)$$

$$\mu_V = \mu_N + 3\sigma^2 .$$

Define the normal distribution function argument x as

$$x = \frac{\ln(D) - \mu_V}{\sigma}$$

where D is particle diameter. Then

$$N(x) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^x \exp(-t^2/2) dt$$

Subroutine DSTBN constructs the particle size class table (i.e., histogram) as follows. Each size class contains a constant

volume fraction,  $\Delta N_V$ , of

$$\Delta N_V = 1/NDSTR .$$

Let  $D_i$ ,  $i = 1, 2, \dots, NDSTR$ , be the upper (i.e. the larger particle) boundary diameter of the  $i$ -th particle size class. The table is ordered with the largest particles in the first size class, and so on. Then, for the  $i$ -th size class

$$N(x_i) = i\Delta N_V$$

and

$$\ln(D_{i+1}) = x_i^\sigma + \mu_V .$$

The upper boundary of the first size class,  $D_1$ , and the lower boundary of the last size class,  $D_{NDSTR+1}$ , are special cases. These are taken to be the diameters at  $\Delta N_V/2$  and  $1-\Delta N_V/2$ , respectively. That is,

$$N(x_1) = \frac{\Delta N_V}{2}$$

and

$$N(x_{NDSTR+1}) = 1 - \frac{\Delta N_V}{2} .$$

In these calculations  $x$  is determined from given  $N(x)$  via equation 26.2.23 of Reference 4.

The central particle diameter for the  $i$ -th class,  $d_i$ , is given by

$$d_i = \sqrt{D_i D_{i+1}} .$$

If NDSTR = 1, a single size class is created with

$$D_1 = (\text{DMEAN}) * (5.0 * \text{SD})$$

$$D_2 = (\text{DMEAN}) / (5.0 * \text{SD})$$

and

$$d_1 = \text{DMEAN}$$

### 3. THE POWER-LAW DISTRIBUTION

#### 3.1 Fundamentals

Mathematically speaking, power-law distributions are meaningless since distribution functions cannot be defined for them. This is because the power-law function is not properly bounded for zero argument. Freiling has shown that fallout particle distributions that have been represented by power-law functions can equally well be fitted by lognormal distribution functions.<sup>(5)</sup> The implication of Freiling's work is that power-law distributions would be more accurately described as truncated lognormal distributions. Nevertheless, power-law distributions frequently are useful in fallout work.

Define the power-law frequency as

$$df(D|k,X) = kD^{-X}dD , \quad (14)$$

where  $df(D|k,X)$  is the number of particles in the diameter range  $D$  to  $D + dD$ . If we assume spherical particles with constant density,  $\rho$ , we have

$$dF\left(D \left| \frac{\pi \rho k}{6M}, X \right.\right) = \frac{\pi \rho k D^{3-X}}{6M} dD , \quad (15)$$

where  $dF\left(D \left| \frac{\pi \rho k}{6M}, X \right.\right)$  is the fraction of the total fallout mass,  $M$ , in the diameter range  $D$  to  $D + dD$ .

The mass fraction of particles in the macro-range from  $D_i$  to  $D_j$  is obtained by integration of Eq. (15) between these limits to give

$$\Delta F = \frac{\pi \rho k}{6M(4-X)} \left( D_j^{4-X} - D_i^{4-X} \right), \quad 0 < X < 4 . \quad (16)$$

### 3.2 Particle Data Analysis

Suppose that we have obtained a sample of fallout particles. We weigh the sample to obtain  $M$  (kg), and we size the sample into  $N$  fractions, the  $i$ -th fraction containing particles in the diameter range  $\Delta D_i$  centered on  $D_i$  (meters). We weigh each fraction and obtain the mass fractions  $\Delta F_i$ . We determine that the average particle density is  $\rho$  ( $\text{kg}/\text{m}^3$ ).

To obtain the power law distribution parameters  $k$  and  $X$ , we plot  $\log(\Delta F_i / \Delta D_i)$  versus  $\log(D_i)$ . A straight line is fitted to the data. From Eq. (15), we see that the intercept and slope are

$$\text{intercept} = c = \log\left(\frac{\pi\rho k}{6M}\right) ,$$

and

$$\text{slope} = m = 3 - X .$$

Then

$$X = 3 - m$$

and

$$k = \frac{6M}{\pi\rho} \log^{-1}(c) .$$

When  $X$  and  $k$  are determined from  $M$  expressed in kilograms,  $D$  and  $\Delta D$  in meters, and  $\rho$  in  $\text{kg}/\text{m}^3$ , they can be input to subroutine LINK1 as EXPO and CAY, respectively.

### 3.3 Particle Size Class Tables

For use in fallout calculations, subroutine DSTBN creates a histogram representation of the power law distribution. The histogram is comprised of NDSTR particle size classes, where NDSTR is

specified by the user. The mass fraction in each size class,  $\Delta F$ , is the constant

$$\Delta F = 1/NDSTR .$$

Let  $D_i$  be the upper (i.e. larger particle) boundary of the  $i$ -th particle size class. The table is ordered with the largest particles in the first class, and so on. Then the smallest particles are contained in the  $NDSTR_{th}$  class. If we assume that the smallest particle in this class is much smaller than  $D_{NDSTR}$ , we see from Eq. (16) that

$$D_{NDSTR}^{4-X} = \frac{6M(4-X)}{\pi\rho k} \Delta F .$$

By recursive use of this relation with Eq. (16), we find that

$$D_i = (NDSTR - i+1)^{\frac{1}{4-X}} D_{NDSTR} .$$

Size class central diameters,  $d_i$ , are

$$d_i = \sqrt{D_i D_{i+1}} .$$

To establish a central and lower boundary diameter for the  $NDSTR_{th}$  class, we say that

$$d_{NDSTR} = \left(\frac{1}{2}\right)^{\frac{1}{4-X}} D_{NDSTR}$$

and

$$D_{NDSTR+1} = (d_{NDSTR})^2 / D_{NDSTR} .$$

#### 4. TABULAR DISTRIBUTIONS

##### 4.1 Particle Size Class Tables

If the user so desires, he can input his particle size distribution in histogram form with NDSTR size classes. The table of size classes must be arranged in descending order of particle diameter. Each size class is defined in the input by its upper (i.e. larger particle) boundary diameter,  $D_i$ , and mass fraction,  $\Delta F_i$ . These two data are punched on a separate card for each size class. The last card in the deck contains the lower boundary diameter of the NDSTRth size class. Central particle diameters,  $d_i$ , are computed to be

$$d_i = (D_i + D_{i+1})/2 .$$

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## 5. USER INFORMATION

### 5.1 Card Input

The ICM card input is described in Table I. This table and the discussions in Sections 2.2, 2.3, 3.2, and 4.1 provide adequate information for use of the code.

### 5.2 Output

Though the printed output has been modified somewhat, the example output presented in DASA-1800-II is still satisfactory.

Communication with the Cloud Rise Module is via COMMON/SET1/. The contents of COMMON/SET1/ is described in Table 2.2 of DASA-1800-III (Revised).<sup>(2)</sup>

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TABLE I  
CARD INPUTS TO THE INITIAL CONDITIONS MODULE

<u>Card Number</u>	<u>Contents</u>	<u>Variable Names and FORMATS</u>
1	ICM Run Identifier	DETID(J), J=1,12 (12A6)
2	Control integer to specify particle size distribution type: 1 lognormal 2 power-law 3 tabular	IDISTR (I5)
3	Number of particle size classes	NDSTR (I5)
4(a)*	(For lognormal particle size distribution) Explosion yield (KT), height of burst above GZ(m), soil class indicator: 1.0 for siliceous 2.0 for calcareous, median particle diameter ( $\mu\text{m}$ ), geometric standard deviation of the particle size distribution, and particle density ( $\text{g}/\text{cm}^3$ ). (See Section 2.2.)	W, HEIGHT, USOIL, DMEAN, SD, DNS (6F10.3)
4(b)*	(For power-law particle size distribution) Yield (KT), height of burst (m), soil class indicator (see above), exponent in the particle size distribution frequency function, coefficient in the particle size distribution frequency function, particle density ( $\text{g}/\text{cm}^3$ ). (See Section 3.2.)	W, HEIGHT, USOIL, EXPO, CAY, DNS (6F10.3)
4(c)*	(For a tabular particle size distribution) Yield (KT), height of burst (m), soil class indicator (see above), particle density ( $\text{g}/\text{cm}^3$ ).	W, HEIGHT, USOIL, DNS (4F10.3)
4(c) <sub>1</sub> ** .	A table of upper boundary particle diameters ( $\mu\text{m}$ ) and mass fractions .	DIAM(J), FMASS(J), J=1,NDSTR (2E12.5) .
4(c) <sub>NDSTR+1</sub> **	The lower boundary diameter ( $\mu\text{m}$ ) of the last particle size class. (See Section 4.1.)	DIAM(NDSTR+1) (E12.5)

Table I (continued)

Card Number	Contents	Variable Names and FORMATS
5	Number of entries in the wind data table	NHODO (I5)
6***	For each entry in the wind data table: altitude (m, relative to msl), x component of wind (m/sec), y component of wind (m/sec)	ZV(J), VX(J), VY(J), J=1, NHODO (3F12.3)

- \* One of the cards 4(a), 4(b), or 4(c) is read according to whether IDISTR is 1, 2, or 3.
- \*\* These cards are read only for a tabular distribution.
- \*\*\* These cards are read only if NHODO > 0.

## 6. FORTRAN STATEMENT LISTINGS

Complete FORTRAN statement listings are given for the following subroutines. These subroutines are operational on the UNIVAC 1108.

<u>SUBROUTINE</u>	<u>Page</u>
LINK1	22
DSTBN	27
SHVIND	29

The machine used to prepare these listings prints a # symbol to represent a 4-8 punch; this symbol should be an apostrophe ('). In FORMAT and DATA statements, the apostrophe is used to define Hollerith character fields.

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C SUBROUTINE LINK1  
 C INITIAL CONDITIONS (FIRBALL) MODULE  
 C MT. AUBURN RESEARCH ASSOCIATES JANUARY 1972  
 C \*\*\*\*\*  
 C  
 C PROGRAM TO DETERMINE THE INITIAL CONDITIONS SPECIFICATIONS OF  
 C TIME, TEMPERATURE, TOTAL SOIL MASS, FRACTION OF THE SOIL PURGED IN  
 C THE VAPOR PHASE, AND THE SIZE FREQUENCY DISTRIBUTION OF THE  
 C CONDENSED PHASE SOIL  
 C  
 C THE FIRST CARD CONTAINS ANY ARBITRARY ALPHANUMERIC IDENTIFICATION.  
 C  
 C OTHER INPUT PARAMETERS ARE - TEST PARAMETER (IDISTR) TO DETERMINE  
 C IF THE PARTICLE SIZE FREQUENCY DISTRIBUTION IS LOG-NORMAL, POWER  
 C LAW, OR TABULAR, YIELD IN KILOTONS, HEIGHT(DEPTH) OF BURST IN  
 C METERS, A SOIL TYPE INDICATOR, FALLOUT PARTICLE DENSITY(GM/CM\*\*3),  
 C MEAN(MICROMETERS) AND STANDARD DEVIATION FOR A LOG-NORMAL PARTICLE  
 C SIZE FREQUENCY DISTRIBUTION, THE NUMBER OF PARTICLE SIZE CLASSES  
 C IN THE PARTICLE SIZE FREQUENCY DISTRIBUTION. IF EITHER A TABULAR  
 C OR POWER LAW DISTRIBUTION IS USED, THE MEAN AND STANDARD  
 C DEVIATION ARE NOT CALLED FOR SINCE THEY DO NOT APPLY. IF A  
 C LOG-NORMAL DISTRIBUTION IS TO BE SUPPLIED BY THE PROGRAM, THE  
 C MEAN AND STANDARD DEVIATION FIELDS ARE LEFT BLANK.  
 C SHOT TIME WINDS ABOVE GZ ALSO ARE INPUT. THESE ARE USED TO  
 C COMPUTE WIND SHEAR EFFECTS ON CLOUD RISE AND FALLOUT ADVECTION  
 C DURING THE CLOUD RISE TIME INTERVAL.  
 C  
 C FOR UNDERGROUND BURSTS INPUT DEPTH OF BURST AS A NEGATIVE NUMBER  
 C  
 C THE OUTPUT UNITS ARE MASS IN KILOGRAMS, LENGTH IN METERS, TIME IN  
 C SECONDS, TEMPERATURE IN DEGREES KELVIN, YIELD IN KILOTONS,  
 C DISTRIBUTION PARAMETERS IN MICRONS  
 C \*\*\*\*\* GLOSSARY \*\*\*\*\*  
 C  
 CAY COEFFICIENT OF THE FREQUENCY FUNCTION FOR THE POWER LINK1 37  
 C LAW PARTICLE SIZE FREQUENCY DISTRIBUTION LINK1 38  
 DETID(I) INITIAL CONDITIONS IDENTIFICATION ARRAY LINK1 39  
 DIAM(I) ARRAY(201), UPPER BOUNDARY OF THE I-TH PARTICLE SIZE LINK1 40  
 C CLASS. THE LAST ENTRY IN THE DIAM ARRAY IS THE LOWERLINK1 41  
 C BOUNDARY OF THE LAST(SMALLEST) PARTICLE SIZE CLASS. LINK1 42  
 C THE LENGTH OF THE DIAM ARRAY IS ALWAYS ONE GREATER  
 C THAN THE NUMBER OF SIZE CLASSES(MICROMETERS) LINK1 43  
 DMEAN MEDIAN DIAMETER (MICROMETERS) OF LOGNORMAL PARTICLE LINK1 44  
 C SIZE DISTRIBUTION LINK1 45  
 DNS FALLOUT PARTICLE DENSITY (GM/CM\*\*3) LINK1 47  
 EXPO EXPONENT OF THE FREQUENCY FUNCTION FOR THE POWER LINK1 48  
 C LAW PARTICLE SIZE FREQUENCY DISTRIBUTION LINK1 49  
 FMASS(I) ARRAY OF FRACTION OF TOTAL PARTICULATE MASS IN I-TH  
 C PARTICLE SIZE CLASS. MAXIMUM LENGTH OF ARRAY = 200 LINK1 50  
 HEIGHT HEIGHT OF BURST (METERS) ABOVE GROUND ZERO LINK1 51  
 IDISTR CONTROL INTEGER FOR PARTICLE SIZE DISTRIBUTION  
 C 1 - LOGNORMAL DISTRIBUTION LINK1 52  
 C 2 - POWER LAW DISTRIBUTION LINK1 53  
 C 3 - TABULAR DISTRIBUTION READ IN ON CARDS (ARRAY WHY)LINK1 54  
 C IS CONTROL INTEGER SPECIFIES WHETHER LOGNORMAL  
 C DISTRIBUTION IS SPECIFIED BY THE USER OR BY THE LINK1 55  
 C  
 C

C	PROGRAM	LINK1 59
C	0 - PROGRAM SPECIFIED LOG-NORMAL DISTRIBUTION	LINK1 60
C	1 - USER SPECIFIED LOG-NORMAL DISTRIBUTION	LINK1 61
C	ISIN	LINK1 62
C	ISOUT	LINK1 63
C	NDSTR	LINK1 64
C	NHODO	LINK1 65
C	PS(I)	LINK1 66
C	SD	LTK1 67
C	SSAM	LINK1 68
C	TME	LINK1 69
C	TMP1	LINK1 70
C	TMP2	LINK1 71
C	T2M	LINK1 72
C	USOIL	LINK1 73
C	VPR	LINK1 74
C	VX(I)	LINK1 75
C	VY(I)	LINK1 76
C	W	LINK1 77
C	ZSCL	LINK1 78
C	ZV(I)	LINK1 79
C	*****	LINK1 80
C	COMMON /SET1/	LINK1 81
C	1CAY ,DETID(12) ,DIAM(201) ,DMEAN ,DNS ,EXPO ,LINK1 91	LINK1 92
C	2FMASS(200) ,IDISTR ,IEXEC ,IRISE ,ISIN ,ISOUT ,LINK1 93	LINK1 93
C	3NDSTR ,PS(200) ,SD ,SSAM ,TME ,TMP1 ,LINK1 94	LINK1 94
C	4TMP2 ,T2M ,USOIL ,VPR ,W ,HEIGHT ,LINK1 95	LINK1 95
C	5ZSCL ,NHODO ,ZV(200) ,VX(200) ,VY(200) ,LINK1 96	LINK1 96
C	*****	LINK1 97
C	FORMAT(12A6)	LINK1 98
1	FORMAT(/3X,60HTHE SPECIFIED STANDARD DEVIATION IS NEGATIVE HENCE INCORRECT//)	LINK1 99
2	FORMAT(13HSOIL CATEGORY)	LINK1100
3	FORMAT(1H+,65X,9HSILICEOUS)	LINK1101
4	FORMAT(1H+,65X,10HCALCAREOUS)	LINK1102
5	FORMAT(1H+,65X,24HHEIGHT OR DEPTH OF BURST,21X,E12.5,2X,6HMETERS/20X)	LINK1103
6	FORMAT(1H+,65X,25X28H**** INPUT PARAMETERS ****/20X,5HYIELD,40X,E12.5)	LINK1104
7	FORMAT(1H+,65X,25X28H**** INPUT PARAMETERS ****/20X,5HYIELD,40X,E12.5)	LINK1105
8	FORMAT(1H+,65X,11HTHE PROGRAM)	LINK1106
9	FORMAT(1H+,65X,8HTHE USER)	LINK1107
10	FORMAT(15I)	LINK1108



```

220 READ(ISIN,3)W,HEIGHT,USOIL,EXPO,CAY,DNS           LTNK1175
      GO TO 23
211 READ(ISIN,3)W,HETGHT,USOIL,DNS                LINK1176
      READ(ISIN,195)(DIAM(I),FMASS(I),I=1,NODSTR)
      LD=NODSTR+1
      READ(ISIN,195)DIAM(LD)                         LINK1177
      LINK1178
      LINK1179
      LINK1180
      LINK1181
C      CHECK ORDERING OF THE HISTOGRAM TABLE          LINK1182
      DO 215 I=2,LD
      IF(DIAM(I) .LT. DIAM(I-1)) GO TO 215
      WRITE( ISOUT,198)
      GO TO 190
215 CONTINUE                                         LINK1183
      LINK1184
      LINK1185
      LINK1186
      LINK1187
C      23 CONVERT HOB - DOB FROM METERS TO FEET       LTNK1188
      23 HEIGHT=HEIGHT/0.3048                          LTNK1189
C      ZSCL IS THE SCALED HOB - DOB                  LINK1190
      60 ZSCL=HEIGHT/((W)**(1.0/3.4))                LINK1191
      LINK1192
      LINK1193
C      TEST THE DATA TO SEE IF THE MODEL IS APPROPRIATE
      IF(HEIGHT)66,66,63                            LINK1194
      63 IF(ZSCL-190.0)170,70,150                  LINK1195
      66 IF(ZSCL+20.0)143,70,70
70      CALL TIME                                     LINK1196
      CALL TEMP                                      LINK1197
      CALL MASS                                      LINK1198
      CALL VAPOR                                      LINK1199
      GO TO (90,95,95),IDISTR                      LINK1200
      LINK1201
      LINK1202
      LINK1203
      LINK1204
      LINK1205
      LINK1206
      LINK1207
      LINK1208
      LINK1209
      LINK1210
      LINK1211
      LINK1212
      LINK1213
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      LINK1217
      LINK1218
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      LINK1222
      LINK1223
      LINK1224
      LINK1225
      LINK1226
      LINK1227
      LINK1228
      LINK1229
      LINK1230
      LINK1231
      LINK1232
C      TEST FOR ACCEPTABLE SPECIFICATIONS OF PRE-SHOT PARTICLE SIZE
C      FREQUENCY DISTRIBUTION.
90      IF(SD)91,92,92                                LINK1206
91      WRITE( ISOUT,2)                               LINK1207
      GO TO 190
92      IF(DMEAN)94,95,95                           LINK1208
94      WRITE( ISOUT,17)
      GO TO 190
C      95      CALL DSTBN                             LINK1210
C      CONVERT HOB - DOB PACK TO METERS FROM FEET
      HEIGHT=HEIGHT*0.3048                          LINK1211
      LINK1212
      LINK1213
      LINK1214
      LINK1215
      LINK1216
      LINK1217
      LINK1218
      LINK1219
      LINK1220
      LINK1221
      LINK1222
      LINK1223
      LINK1224
      LINK1225
      LINK1226
      LINK1227
      LINK1228
      LINK1229
      LINK1230
      LINK1231
      LINK1232
C      WRITE INITIAL CONDITIONS RESULTS
      WRITE( ISOUT,4)W,HEIGHT
      IF(USOIL-1.0)301,301,302
301     WRITE( ISOUT,5)
      GO TO 305
302     WRITE( ISOUT,6)
305     GO TO (309,310,311),IDISTR
309     WRITE( ISOUT,7)DMEAN,SD
      IF (IS)102,103,102

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103 WRITE (ISOUT,9) LINK1233
    GO TO 315 LINK1234
102 WRITE (ISOUT,9) LINK1235
    GO TO 315 LTNK1236
  311 WRITE (ISOUT,19) NDSTR LTNK1237
C           PRINT FINAL PARTICLE SIZE CLASS LINK1238
C
  315 WRITE (ISOUT,193) LINK1239
    DO 602 J=1,NDSTR LINK1240
    J0=J+1
    DM1=DIAM(J0)*1.0E-6
    DM2=DIAM(J)*1.0E-6
  602 WRITE (ISOUT,194) J,PS(J),DM1,FMASS(J),DM2 LINK1241
    GO TO 106 LTNK1242
  310 WRITE (ISOUT,197) NDSTR,CAY,EXPO LINK1243
    GO TO 315 LINK1244
106 WRITE (ISOUT,13) TME,TMP1,TMP2,VPR,SSAM LINK1245
118 WRITE (ISOUT,192) LTNK1251
200 CALL SHWIND
    WRITE (ISOUT,15) LINK1252
    RETURN
    LINK1253
143 WRITE (ISOUT,11) LINK1254
    GO TO 190
150 WRITE (ISOUT,12) LINK1255
190 CALL EXIT
    END
    LINK1256
    LINK1257
    LINK1258
    LINK1259

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```

SUBROUTINE DSTBN
COMMON /SET1/
1CAY      ,DEFID(12) ,DIAM(201) ,DMEAN      ,DNS      ,FXPO      ,DSTBN    1
2FMASS(200),IDISTR   ,IEXEC      ,IRISE      ,ISIN      ,ISOUT     ,DSTBN    2
3NDSTR    ,PS(200)   ,SD        ,SSAM       ,TME       ,TMPI      ,DSTBN    3
4TMP2     ,T2M       ,USOIL     ,VPR       ,W         ,HEIGHT    ,DSTBN    4
5ZSCL     ,NH000     ,ZV(200)   ,VX(200)   ,VY(200)   ,          ,DSTBN    5
                                         ,          ,          ,          ,          ,DSTBN    6
                                         ,          ,          ,          ,          ,DSTBN    7
                                         ,          ,          ,          ,          ,DSTBN    8
                                         ,          ,          ,          ,          ,DSTBN    9
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                                         ,          ,          ,          ,          ,DSTBN   11
                                         ,          ,          ,          ,          ,DSTBN   12
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                                         ,          ,          ,          ,          ,DSTBN   57
                                         ,          ,          ,          ,          ,DSTBN   58

C
C LOGNORMAL DISTRIBUTION TO 100
C POWER FUNCTION DISTRIBUTION TO 200
C TABULAR DISTRIBUTION TO 300
C

C EQUATION 26.2.23 OF NBS-AMS 55 HANDBOOK IS USED TO COMPUTE THE
C PROBABILITY FUNCTION ARGUMENT FROM THE RATIONAL POLYNOMIAL
C APPROXIMATION TO THE NORMAL PROBABILITY FUNCTION.
C
C TA(X)=SQT(ALOG(1.0/X**2))
C APX(X)=TA(X)-(2.515517+0.802853*TA(X)+0.010323*TA(X)**2)/
C (1.0+1.432799*TA(X)+0.139269*TA(X)**2+0.001308*TA(X)**3)
C LD=NDSTR+1
C GO TO (100,200,300),IDISTR
100 IF(DMEAN)111,111,112
111 DMEAN=0.407
SD=4.0
112 IF(NDSTR-1)101,101,102
101 PS(1)=DMEAN*1.0E-6
C5=SD**5
DIAM(1)=DMEAN*C5
DIAM(2)=DMEAN/C5
FMASS(1)=1.0
GO TO 400
102 BARMU=ALOG(DMEAN)
SIGMA=ALOG(SD)
BARMU=BARMU+3.*SIGMA**2
FRAC=1.0/FLOAT(NDSTR)
DO 103 ND=1,NDSTR
103 FMASS(ND)=FRAC
NH=NDSTR/2
DO 104 I=1,NH
PRR=FLOAT(I)*FRAC
DIAM(I+1)=BARMU+APX(PRR)*SIGMA
J=NDSTR-I+1
104 DIAM(J)=BARMU-APX(PRR)*SIGMA

C
C FOR THE 2 EXTREME INTERVALS THE AVERAGE DIAMETER IS
C ASSUMED TO BE AT HALF A MASS FRACTION FROM ZERO AND ONE
C
PRB=FRAC/2.0
PS(1)=BARMU+APX(PRB)*SIGMA
PS(NDSTR)=BARMU-APX(PRB)*SIGMA
DIAM(1)=2.*PS(1)-DIAM(2)
DIAM(LD)=2.*PS(NDSTR)-DIAM(NDSTR)

C
C CALCULATE MEAN DIAMETERS FROM BOUNDARY VALUES.
C
J=NDSTR-1
IF(J-1)107,107,105
105 DO 106 I=2,J
106 PS(I)=0.5*(DIAM(I)+DIAM(I+1))


```

```

107 DO 108 I=1,NDSTR          DSTBN 59
  DIAM(I)=EXP(DIAM(I))        DSTBN 60
108 PS(I)=EXP(PS(I))*1.0E-6   DSTBN 61
  DIAM(LD)=EXP(DIAM(LC))     DSTBN 62
  GO TO 400                   DSTBN 63
200 IF(EXPO<4.0)201,202,202  DSTBN 64
202 WRITE(ISOOUT,2001)        DSTBN 65
  CALL EXIT                   DSTBN 66
2001 FORMAT('#1#,1X,*EXONENT OF POWER LAW POWER LAW PARTICLE SIZE FREQUENCIES')
1ENCY DISTRIBUTION GT. OR EQ. 4.0#)  DSTBN 67
201 IF(NDSTR>1)203,204,204  DSTBN 68
203 NDSTR=10                  DSTBN 69
204 AN=FLCAT(NDSTR)          DSTBN 70
  FRAC=1.0/AN                DSTBN 71
  DO 205 I=1,NDSTR          DSTBN 72
205 FMASS(I)=FRAC           DSTBN 73
  POW=1.0/(4.0-EXPO)         DSTBN 74
  DMIN=(6.0*SSAM*FRAC/(POW*CAY*DNS*3.14159E6))**POW
  DO 206 IJ=1,NDSTR         DSTBN 75
  AJ=FLOAT(IJ)-1.0           DSTBN 76
206 DIAM(IJ)=(AN-AJ)**PCW*DMIN  DSTBN 77
  PS(NDSTR)=DMIN*0.5**POW    DSTBN 78
  DIAM(LD)=PS(NDSTR)**2/DIAM(NDSTR)
  ND=NDSTR-1                 DSTBN 79
  DO 207 IJ=1,ND             DSTBN 80
207 PS(IJ)=SQRT(DIAM(IJ)*DIAM(IJ+1))
  DO 208 IJ=1,L0             DSTBN 81
208 DIAM(IJ)=1.0E+6*DIAM(IJ)  DSTBN 82
  GO TO 400                   DSTBN 83
300 DO 301 I=1,NDSTR         DSTBN 84
301 PS(I)=0.5*(DIAM(I)+DIAM(I+1))*1.0E-6
400 RETURN                   DSTBN 85
  END                         DSTBN 86
                                DSTBN 87
                                DSTBN 88
                                DSTBN 89
                                DSTBN 90
                                DSTBN 91

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C          SUBROUTINE SHWIND
C          READS IN SHOT TIME WIND DATA ABOVE GROUND ZERO
C
COMMON /SET1/
1CAY      ,DETID(12) ,DIA1(201) ,DMEAN      ,DNS        ,EXPO      ,SHWND 1
2FMASS(200),IDISTR   ,IFXEC      ,IRISE      ,ISIN       ,ISOUT     ,SHWND 2
3NDSTP    ,PS(200)   ,SD         ,SSAM       ,TME        ,TMP1      ,SHWND 3
4TMP2     ,T24        ,USOIL      ,VPR        ,W          ,HEIGHT    ,SHWND 4
5ZSCL     ,NHODO     ,ZV(200)    ,VX(200)    ,VY(200)   ,SHWND 5
READ(ISIN,1)NHODO
IF(NHODO)100,100,200
100 WRITE(ISOUT,5)
GO TO 300
200 READ(ISIN,2)(ZV(J),VX(J),VY(J),J=1,NHODO)
  WRITE(ISOUT,3)NHODO
  WRITE(ISOUT,4)(ZV(J),VX(J),VY(J),J=1,NHODO)
300 RETURN

1 FORMAT(I5)           SHWND 19
2 FORMAT(F12.3, 2F12.3) SHWND 20
3 FORMAT(1X,2X,2X,WIND HODOGRAPH AT GROUND ZERO,10X,NHODO = I5//1SHWND 21
11X,VECTOR ALTITUDE, ZV(J),16X,VX(J),24X,VY(J)) SHWND 22
4 FORMAT(3(16X,E13.6)) SHWND 23
5 FORMAT(1X,2X,2X,SHOT-TIME WINDS HAVE NOT BEEN SPECIFIED) SHWND 24
END SHWND 25

```

## REFERENCES

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3. J. Aitchison and J. A. C. Brown, The Lognormal Distribution (Cambridge University Press, Cambridge, England, 1966).
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